Use of a Potential Analogue Method for the Design of Electrical

Taking logs of (1):

$$ln S = A + iB = \Gamma$$
(2)

where A - the working attenuation,

B - the working phase change, - the working transfer coefficient.

For the attenuation, we have:

$$A(\lambda) = \ln |s| = \ln \frac{(\lambda - \lambda_1)(\lambda - \lambda_3)...(\lambda - \lambda_{2n-1})}{(\lambda - \lambda_2)(\lambda - \lambda_4)...(\lambda - \lambda_{2m})} \ln H \quad (3).$$

The potential function of a plane electrical field takes the form of an infinite conducting plane, such as a large electrolytic tank with a thin layer of electrolyte. Let two electrodes between which a current I flows dip into the electrolyte.

Then the potential at any point M situated at a distance  $R_1$  from the negative electrode and  $R_2$  from the positive electrode Card 2/13

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is determined (Ref 2) by the formula:

$$U = \frac{I_{\frac{3}{2\pi\gamma l}}}{2\pi\gamma l} \ln \frac{R_{1}}{R_{2}}$$
 (4)

where  $\gamma$  is the conductance of the electrolyte,  $\gamma$  is the depth of the electrolyte.

Two co-ordinates X and Y (Figure 1) are taken on the conducting plane and the electrolyte surface is considered as the plane of a complex variable:

$$z = x + iy$$
.

Then the distance from the point  $\, \, M \,$  to the electrodes is determined by the following:

$$R_1 = |z - z_1|$$
,  $R_2 = |z - z_2|$ 

and substituting in (4), we obtain:

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Use of a Potential Analogue Method for the Design of Electrical

$$U = a \ln \left| \frac{z - z_1}{z - z_2} \right| \tag{5}$$

where

$$a = \frac{I_3}{2\pi\gamma l} \tag{6}$$

is a constant depending on the current in the electrodes and on the conductance and depth of the electrolyte. For a given number of pairs, the potential at any point of the plane Z equals:

$$U(z) = a \ln \left| \frac{(z - z_1)(z - z_3)...(z - z_{2n-1})}{(z - z_2)(z - z_4)...(z - z_{2n})} \right|$$
(7)

where z<sub>1</sub>,..., z<sub>2n-1</sub> are the co-ordinates of the negative electrodes, z<sub>2</sub>,...,z<sub>2n</sub> are the co-ordinates of the positive card4/13

Use of a Potential Analogue Method for the Design of Electrical Filters

If the electrode co-ordinates are chosen so that they are numerically equal to the values of the zeros and the poles of the transfer function, then the analogy between expressions (3) and (7) is complete, except that in the denotation of the variables, the constant multiplier a and the additional term  $\ln H$ . Denoting the independent variable in both expressions by  $\lambda$ , i.e. assuming that the plane of the complex frequency coincides with the plane Z and solving simultaneously Eqs.(3) and (7), we obtain:

$$A(\lambda) = \frac{U(\lambda)}{a} + \ln H \qquad (8) .$$

For a reference level  $\lambda_o$ :

$$A(\lambda_0) = \frac{U(\lambda_0)}{a} + \ln H$$
 (9)

and subtracting Eq.(9) from (8), we have: Card 5/13

Use of a Potential Analogue Method for the Design of Electrical Filters

$$\Delta(\lambda) - \Delta(\lambda_0) = \frac{U(\lambda) - U(\lambda_0)}{a}$$
 (10)

or

$$A = U/a \tag{11}$$

where U is the potential difference measured in the electrolyte between the point  $\lambda$  and the reference point  $\lambda_0$ . A is the difference in the working attenuation at frequencies corresponding to these points. If the current in the electrodes is adjusted so that a equals unity, then A = U, i.e. the potential difference in volts is numerically equal to the working attenuation in nepers. The current in each electrode must equal:

$$I_{\mathbf{a}} = 2 \mathbf{n} \gamma \mathbf{l} \tag{12}$$

A simple method for determination of the frequency characteristic of the working attenuation can be devised on the basis of this mathematical analogue. Positive Card 6/13

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electrodes are placed on the complex frequency plane, which coincides with the electrolyte surface, at points corresponding to the poles of the transfer function and negative electrodes at points corresponding to the zeros of the transfer function. Equal currents determined by Eq.(12) are established in all the electrodes. Then the potential, measured along the real frequency axis relative to the co-ordinate origin will equal the working attenuation in nepers. Any given attenuation can be obtained by changing the positions of the electrodes. Then knowing the zeros and poles, the four-terminal network for the given attenuation can be determined. The character of the field for a half-section of a lowfrequency k type filter is determined and an equation for an ellipse is obtained. Thus, the lines of equal attenuation of a k type half-section will be ellipses. In the potential analogue equipotential lines correspond to lines of equal attenuation. Any equipotential line can act as an electrode and the most convenient electrode will be a plane electrode placed in the electrolytic tank along Card7/13 the real frequency axis from  $-i\omega_1$  to  $+i\omega_2$ .

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Use of a Potential Analogue Method for the Design of Electrical Filters

infinitely distant point can serve for the other electrode, for which the frame of an electrolytic tank of large dimensions can be used. In this case, the electric field will be as shown in Figure 2. The current lines shown dotted are everywhere orthogonal to the equipotential lines, shown in full and form a family of co-focal hyperbolae with focii  $\pm i\omega_1$ .

To determine the frequency-attenuation characteristic of the type k half-section, the potential along the real frequency axis relative to the plane electrode is measured by a cathode voltmeter. If the attenuation of the full type k section is required, then the current in the electrodes must be doubled.

For a type m section, the characteristic transfer constant is determined by the formula:

$$sh \frac{\Gamma_{m}}{2} = \sqrt{\frac{Z_{1m}}{4Z_{2m}}}$$
(19)

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Again, hyperbolic sinusoidal functions are presented with the difference that the right-hand side reaches an infinitely great value not when  $\lambda=\infty$ , but at a specific finite frequency:

$$\lambda_{\infty} = \pm \frac{i\omega_1}{\sqrt{1-m^2}} = \pm i\omega_{\infty}$$
 (20)

corresponding to the attenuation pole of the type m section. To measure the frequency characteristic of the type m section, it is necessary to put one electrode at the point  $+i\omega_{\infty}$  and the other at the point  $-i\omega_{\infty}$ . Current of strength I<sub>3</sub> is passed through each electrode and the total current 2I<sub>3</sub> passes through the plane electrode disposed along the segment  $-i\omega_{1}$ ,  $+i\omega_{1}$ . The potential relative to the plane electrode measured by a cathode voltmeter along the real frequency axis will be proportional to the

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Use of a Potential Analogue Method for the Design of Electrical Filters

characteristic attenuation of the m type section. the filter consists of several m type sections, then electrodes are placed in the electrolytic tank at points on the real frequency axis corresponding to the attenuation poles of the individual sections (Figure 3). The same current I, flows in all the electrodes. Then the potential relative to the plane electrode in volts measured along the real frequency axis will equal the summated attenuation of the filter in nepers. To avoid errors due to the finite dimensions of the electrolytic tank and the physical positioning of the electrodes, it is convenient to transform the complex frequency plane into a rectangle (Ref 3) by using an elliptical integral of the first order. This transformation is written in the form of an elliptical sine function. Then, the whole plane of the complex frequency is transformed into rectangles on the Z plane (Figure 3). In view of the symmetry, it is sufficient to consider only one quadrant transformed into a rectangle on the plane Z with sides K and K' (Figure 4).

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Use of a Potential Analogue Method for the Design of Electrical Filters

The apparatus is illustrated in Figure 5. The base of the tank is a polished sheet of glass 60 x 70 cm and 4 - 5 mm thick. Four plexiglass or ebonite plates, 15 - 20 mm, 5 - 6 mm thick, are fixed to the glass and form the electrolytic tank. The width of the tank corresponds to the side K and equals, for example,  $X_k = 50$  cm. The height of the bath corresponding to side K' equals:

$$Y_{K'} = 50 \quad \frac{K'}{K} \quad cm \qquad (27) \quad .$$

The upper movable plate corresponding to the stop band is fixed in accordance with this dimension. Tap water was used for the electrolyte and the depth was 3 - 4 mm. Thin sewing needles or copper wires 0.5 - 0.6 mm diameter were used for the electrodes. A strip of copper foil secured by screws to the lower fixed plate of the tank formed the plane electrode. The co-ordinates X and Y were read off directly in mm from graph paper under the glass. To avoid polarisation of the electrodes, a 1 000 c.p.s. generator (types 3G-2A or 3G-10) with a 60 V output was used.

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Use of a Potential Analogue Method for the Design of Electrical Filters

For measurement of the potential relative to the plane electrode, a valve voltmeter of type VKS-7B was used. The potential drop across 300 Ω resistors connected in series with each electrode was measured by a high impedance input meter, thereby obtaining the current value. The current in each electrode is adjusted to agree with Eq.(12) and then the voltmeter reading in volts is equal to the attenuation in nepers at the current in the electrodes in the transformed plane is two times less than in the plane Λ (Figure 4) and therefore formula (12) takes the form:

 $I_{\mathbf{j}} = \mathbf{P} \gamma \mathbf{l} \tag{28}.$ 

The elentrode current is, in practice, within the limits 0.5 to 1.5 mA, depending on the salt content of the water and on the depth of the electrolyte.

In Figure 6 is produced the curve of the characteristic attenuation of a filter of class 3, 5 constructed from

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Use of a Potential Analogue Method for the Design of Electrical Filters

measurements taken in an electrolytic tank. There is good agreement between experimental and calculated results. There are 6 figures, 1 table and 6 references, 3 of which are Soviet, 1 German and 2 English.

SUBMITTED: March 11, 1957

Card 13/13 1. Electric filters--Design 2. Mathematics--Applications

sov/106-58-12-7/13

AUTHOR: Ufel man, A.F.

TITLE:

A Theorem on the Mean Value of the Attenuation in the

Stop-Band of a Filter (Teorema o srednem znachenii

zatukhariya v polose zaderzhivaniya fil'tra)

PERIODICAL: Elektrosvyaz, 1958, Nr 12, pp 49 - 57 (USSR)

ABSTRACT: At the present time, the design of electrical filters is based on the simplest case when the required

atternation in the stop-band or in part of the stop-band is constant. In practice, the requirements are often different: in one part of the band, high attenuation is required, but in other parts the attenuation may be significantly less. In these cases, to design the filter giving a guaranteed constant minimum attenuation is uneconomical. The article develope a new theorem, from which simple design formulae can be derived, enabling the optimum filter design to be obtained quickly and accurately. The theorem is formulated as follows: "The

mean value of the characteristic attenuation in the stop-band of a filter expressed in terms of an elliptical

Card 1/2 frequency scale remains constant for a given class of filter with any given distribution of the infinite-

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A Theorem on the Mean Value of the Attenuation in the Stop Band of a Filter

> attenuation frequencies". The article commences with the results obtained by the author (Ref 1) who showed that the complex frequency plane is transformed into rectangles on the z-plane by the expression:

> > $\Lambda = i \operatorname{sn}(z, k)$

where  $\Lambda = \Sigma + i \Omega$  - normalized complex frequency,

- normalized frequency, - cut-off frequency.

The design formulae derived are also applicable to the working attenuation, but the proof of this is to be the subject of a separate article.

There are 3 figures, 1 table and 3 Soviet references. SUBMITTED: March 21, 1958.

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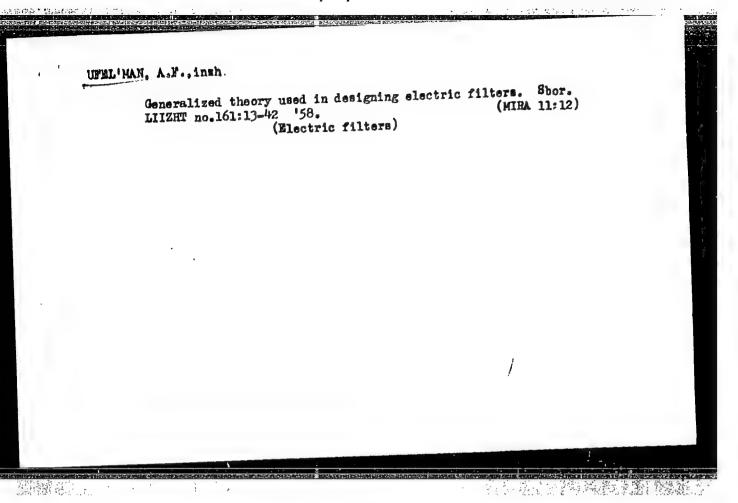
## "APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001857820007-3

UFEL'MAN, A.F., assistent

Zlotarev's fraction and its use in designing filters by means of characteristic parameters. Sbor. LIIZHT no.158:387-408 \*58.

(Electric filters)

(Electric filters)



#### UFER MAN. A.F.

Generalized theory on Chebyshev reactive filters. Izv. vys. ucheb. zav.; radiotekh. 2 no.6:679-693 N-D '59. (MIRA 13:6)

1. Rekomendovana kafedroy elektrosvyazi Ural'skogo elektromekhanicheskogo instituta i zhenerov zheleznodoroshnogo; transporta: . (Electric filters)

AUTHOR: Ufel'man, A.F. SOV/106-59-7-9/16

TITLE: The General Law for the Position of the Roots of the Characteristic Polynomial in the Complex Frequency Plane for the Design of Filters for the "Working" Parameters

PERIODICAL: Elektrosvyaz', 1959, Nr 7, pp 57 - 65 (USSR)

ABSTRACT: The "working" parameters of a four-terminal network, consisting of a finite number of lumped elements, can be expressed by three real polynomials, f, g, h of the complex frequency  $\lambda = 6 + \frac{1}{2}\omega$ :

 $S = \frac{g}{f}, \quad W = \frac{g + h}{g - h} \tag{1}$ 

where S is the working transfer coefficient; W is the normalised input impedance.

Also:

 $e^{2A} = 1 + |\varphi|^2 \tag{2}$ 

where A = log |S| is the working attenuation of the fourterminal network;

Cardl/6  $\varphi = h/f$  is the "filtration" function.

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The General Law for the Position of the Roots of the Characteristic Polynomial in the Complex Frequency Plane for the Design of Filters for the "Working" Parameters

For reactive four-terminal networks, the polynomials are related by:

$$g(\lambda)g(-\lambda) = f(\lambda)f(-\lambda) + h(\lambda)h(-\lambda)$$
 (3).

The polynomials f, g, h are the simplest and most universal characteristics of a four-terminal network since, if these polynomials are known, both the working and characteristic parameters of the network can be found and also its circuit determined.

The problem of synthesis of an electric filter according to its working attenuation consists of finding a filter circuit with the minimum number of elements to give a working attenuation in the passband smaller than some value  $\mathbf{A}_{\max}$  and in the stopband greater than  $\mathbf{A}_{\min}$ .

This problem can be divided into three parts:

reconstruction and a design and a construction of the construction

1) The problem of finding the best approximation to the given requirements of the working attenuation, using a

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The General Law for the Position of the Roots of the Characteristic for the "Working" Parameters

fractional rational  $\varphi = h/f$  of the lowest possible degree.

2) Determination of the polynomial  $g(\lambda)$  by Eq (3). 3) Determination of the filter circuit according to the polynomials found (f, g, h).

The first and third problems have been examined in the references quoted but determination of the polynomial  $g(\lambda)$  presents great difficulty. The roots of the polynomial  $g(\lambda)$  are equal to the roots of the characteristic equation of the system and correspond to the frequencies of free oscillations which can arise in a loaded four-terminal network. Therefore,  $g(\lambda)$  is called the characteristic polynomial of the four-terminal network. Since in passive four-terminal networks, the free oscillations must decay, the real part of the roots of  $g(\lambda)$  must be negative. This enables the polynomial  $g(\lambda)$  to be determined by the known roots of the righthand part of Eq (5); all the roots with a negative real part correspond to the polynomial

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The General Law for the Position of the Roots of the Characteristic Polynomial in the Complex Frequency Plane for the Design of Filters for the "Working" Parameters

and with a positive real part the polynomial  $g(-\lambda)$  . Thus, the entire problem is to find the roots of the righthand part of Eq (3). A method is developed in the article for finding the roots of the characteristic polynemial, based on using the special properties of the filtration" function, which for filters is a rational Chebyshev function. The properties of Chebyshev functions enable these functions to be used for the design of electrical functions. Other conditions being equal, they ensure the maximum possible working attenuation in the stopband. The Chebyshev functions can be simply represented by a "comparison" filter, which is a filter in which the characteristic attenuation poles coincide with the poles of the given Chebyshev function. Figure 5 shows a Chebyshev function of the fifth degree obtained by using a comparison filter, consisting of two matype sections and one k-type half-section.

Card4/6 It is shown that rational Chebyshev functions can be uniquely

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The General Law for the Position of the Roots of the Characteristic Polynomial in the Complex Frequency Plane for the Design of Filters for the "Working" Parameters

> represented by using a comprison filter. On this basis a general law for the distribution of the roots of the characteristic polynomial in the complex frequency plane is found. The roots of the polynomial  $g(\lambda)$  are situated in the left half of the A splane at points of intersection of the lines of equal attenuation of the comparison filter at which the characteristic attenuation equals:

$$A_{N} = Ar sh \frac{1}{\sqrt{2A_{max} - 1}}$$

with the lines of equal phase, which unite each pole of the Chebyshev function with the corresponding zero. Using the conform transformation of the complex frequency plane, the exact design formulae for determination of the roots can be obtained for the case when the filtration is a Zolotarev fraction and the simple approximation

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### "APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001857820007-3

The General Law for the Position of the Roots of the Characteristic Polynomial in the Complex Frequency Plane for the Design of Filters for the "Working" Parameters

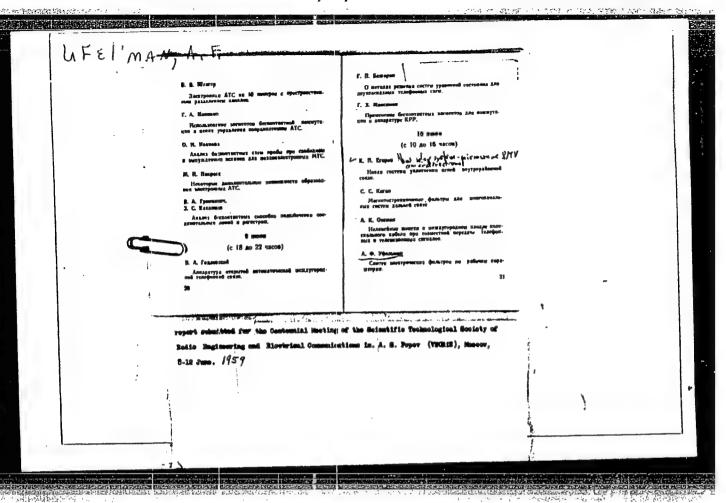
formulae for the general case when the filtration function is a Chebyshev fraction.

There are 3 figures and 10 references, of which 7 are Soviet, 2 German and 1 American.

SUBMITTED: March 10, 1959

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# "APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001857820007-3



26211 s/106/60/000/003/003/003 A055/A133

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AUTHOR:

Ufel'man, A.F.

TITLE:

Determination of the roots of the characteristic polynomial of Che-

byshev filters

PERIODICAL: Elektrosvyaz', no. 3, 1960, 44 -51

TEXT: In a previous work [Ref. 3: Raschet elektricheskikh filtrov s pomoshch'yu potentsial noy analogii. Kandidatskaya dissertatsiya. (Calculation of electrical filters with the aid of potential analogy. Candidate's Dissertation.) LIIZMT, 1957], the author showed that if the filtration function is a Zolotarev fraction, the disposition of the characteristics polynomial roots proves to be the simplest in the conformally transformed plane z related to the complex frequency plane by the equation:  $\Lambda = \sinh(z, k)$ , (2) where  $\Lambda = \Sigma + i\Omega$  is the normalized complex frequency;  $\Omega = \frac{\omega}{\omega_1} = \frac{1}{f_1}$  is the normalized frequency;  $\Omega = \frac{1}{f_2}$ 

is the cutoff steepness,  $f_1$  is the boundary frequency of the pass band and  $f_2$  the boundary frequency of the cutoff band. The arrangement of the roots in plane z becomes particularly clear if potential analogy is used. In his previous work, the author showed that the equi-attenuation lines in plane  $\Lambda$  correspond to equi-

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potential lines in an electrolytic tank, and that equiphase lines correspond to current lines. The roots of the polynomial g ( $\Lambda$ ) are located in the intersection points of the equipotential line U = AN with the mean current lines starting from each electrode. In the case of a Zolotarev fraction, the mean current lines are parallel to axis y and the equipotential line  $U = A_N$  is parallel to axis x. The purely experimental method of determining the roots of the polynomial g ( $\Lambda$ ), such as it is described by Boothroyd, proved very labor-consuming and insufficiently accurate. The author suggests, therefore, an analytical approximate method based upon the following postulates: 1) In plane z, the characteristic line is considered a straight line and is, therefore, determined by two points (0,  $y_{\Sigma}$ ) and (K,  $y_{\Omega}$ ), corresponding to the characteristic frequencies  $\Sigma_N$  and  $\Omega_N$ . 2) The equiphase lines intersect the characteristic line and the x-axis at right angles and are consequently assimilated to circle-arcs with the center located in the intersection point of the prolonged characteristic line with the x-axis. The intersection points with the x-axis of the equiphase lines on which the roots of the polynomial g ( $\Lambda$ ) located are the zeros of the Chebyshev fraction. The characteristic frequencies  $\Sigma_N$  and  $\Omega_N$  at which the attenuation of the comparison filter is equal to  $A_N$  can also be easily determined. The determination of the ordinates  $y_\Sigma$  and  $y_Q$  is particularly simple if potential analogy is used. The

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Determination of the roots of the characteristic....

slope of the characteristic line is determined by:  $tg\gamma = \frac{\Delta y}{K}$ ,  $\Delta y = y_{\Sigma} - y_{\Omega}$ ,  $\Im$  where K is the full elliptical integral of the first kind with modulus k. The shift of the abscissae of the roots of  $\Lambda$  with respect to the zeros of the Chebyshev fraction x is  $\Delta x_{\gamma} = R_{\gamma} - R_{\gamma} \cos \gamma$ , (4) where  $R_{\gamma} = a + (K - x_{O_{\gamma}})$ , (5). Substituting the radius of curvature  $R_{\gamma}$  in (4), the author obtains:  $\Delta x_{\gamma} = K(1 - \cos \gamma) \left( \frac{y_{\Omega}}{\Delta y} + 1 - \frac{x_{O_{\gamma}}}{K} \right).$ 

(6)

The coordinates of the roots of the characteristic polynomial in plane z are  $\text{de}_{\overline{x}}$ termined by the following formulae:  $x_v = x_{0v} + \Delta x_v$ , (7):  $y_v = y_0 + \Delta y$  (1 -  $\frac{\lambda v}{K}$ ) (8). This method can be named the "three points method". Substitution of the thus found values of the coordinates  $z_{y} = x_{y} + i y_{y}$  in (2) results in:  $\Delta_{y} = \Sigma_{y} + i \Omega_{y} = i \text{ sn } (x_{y} + i y_{y}, k)$ , (9). Starting from this formula, it is easy to obtain the roots of the polynomial g ( $\Lambda$ ):

 $Q_{y} = \frac{\operatorname{sn} x \operatorname{dn} y}{\operatorname{cn}^{2} y + (k \operatorname{sn} x \operatorname{sn} y)^{2}}.$  (11)  $\sum_{y} = -\frac{\operatorname{cn} x \operatorname{dn} x \operatorname{sn} y \operatorname{cn} y}{\operatorname{c} n^{2} y + (\operatorname{ksn} x \operatorname{sn} y)^{2}}, \quad (10);$ 

Formulae (10) and (11) require, however, a labor-consuming interpolation and are,

therefore, difficult to use. Using transformations, the author obtains:  $\Sigma_0 = - T_{\nu} \frac{b_{\nu}}{1 + a_{\nu}} , \qquad \Omega_{\nu} = S_{\nu} \frac{c_{\nu}}{1 + a_{\nu}} .$ (12)

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Determination of the roots of the characteristic....

where  $S_{\nu} = \operatorname{sn}(x_{\nu}, k)$ ,  $T_{\nu} = \operatorname{tn}(y_{\nu} k')$ , (13);  $a_{\nu} = k^2 T_{\nu}^2 S_{\nu}^2$ ,  $b_{\nu} = \sqrt{(1 - S_{\nu}^2)(1 - k^2 S_{\nu}^2)}$ , (14);  $c_{\nu} = \sqrt{(1 + T_{\nu}^2)(1 + k^2 T_{\nu}^2)}$ , (15). S, can be expressed in terms of the Chebyshev fraction zeros  $\Omega_{0\nu}$ , and  $T_{\nu}$  in terms of  $\Sigma_{N}$  and  $\Omega_{N}$  with the aid of the following formulae (derived by the author in an appendix to the article):  $S_{\nu} = \Omega_{0\nu} + \Delta x_{\nu} b_{0\nu}$ , (16);  $T_{\nu} = \sum_{N} - (\sum_{N} - T_{\nu}) \frac{x_{\nu}}{K}$  (17); where  $b_{0\nu} = \sqrt{(1 - \Omega_{0\nu}^2)(1 - k^2 \Omega_{0\nu}^2)}$ , (18);  $T_{\Omega} = \sqrt{\frac{\Omega_{0\nu}^2 N^{-1}}{1 - k^2 \Omega_{0\nu}^2}}$ , (19)

The roots of polynomial g  $(\Lambda)$  can thus be determined with the aid of formulae (12) if the following magnitudes are known: the zeros of the Chebyshev fraction  $\Omega_0$ , the characteristic frequencies  $\Sigma_N$  and  $\Omega_N$ , and the abscissae shift  $\Delta x$ , in plane z [calculated with formula (6)]. The accuracy of formulae (12) depends on the magnitude of the shift of the attenuation poles from the "iso-extremal" position. When this shift is equal to zero,  $\Delta x_{\nu} = 0$ ;  $S_{\nu} = \Omega_{0\nu}$ ;  $T_{\nu} = \Sigma_{N}$ , and formulae are obtained that are accurate for cases when the filtration function is a Zolotarev fraction. It is possible to simplify the above derived formulae by eliminating  $\Delta x_{\nu}$  from (16) and  $x_{\nu}$  from (17). Resorting to the relation:  $\frac{x_{\nu}}{K} \approx \frac{n - (2\nu - 1)}{n}$ .

(21)

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where n is the power of the Chebyshev fraction, and substituting (21) in (17), the

$$T_{0y} = \sum_{N} - (\sum_{N} - T_{Q}) \frac{n - (2y - 1)}{n}$$
(22)

The correction  $\Delta x_{s}$ ,  $b_{0}$  in (16) does not represent more than 1-2%; therefore, it is possible to state that:  $S_{s} \approx \Omega_{0}$ . Taking all this into consideration, the author writes the simplified formulae for the determination of the polynomial roots

$$\sum_{y} = -T_{0y} \frac{b_{0y}}{1 + a_{0y}}, \qquad \Omega = \Omega_{0y} \frac{a_{0y}}{1 + a_{0y}}, \qquad (23)$$

Where:

$$a_{0,} = k^{2} T_{0,}^{2} \Omega_{0,}^{2} \qquad (24) \qquad \text{and} \qquad c_{0,} = \sqrt{(1 + T_{0,}^{2})(1 + k^{2} T_{0,}^{2})}. \tag{23}$$
Ing established these formula

Having established these formulae, the author applies them in a numerical example, and, finally, draws the following conclusions: When approximate formulae (23) are used for the calculation (with the aid of a slide-rule), the error varies within 0.5+5 % depending on the degree of the irregularity of the conditions set on the

Card 5/6

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Determination of the roots of the characteristic .... oparating attenuation in the cutoff-band of the filter. When this irregularity  $\mu$ is below 0.05, the roots must be calculated using formulae (12) (with the aid of an arithmometer) or formula (10) and (11) (with the aid of elliptical function tables). If the irregularity is large, the error with formulae (12) can reach 1 - 3%. In that case, it is necessary to render the determination of the roots more precise resorting to one of the well-known methods, for instance to that described by Cauer [Ref. 6: "Theorie der linearen Wechselstromschaltungen", Berlin, 1954). There are 4 figures and 7 references, 4 Soviet-bloc and 3 non-Soviet-bloc. The 2 English language references are: Boothroyd. "Design of electric wave filters with the aid of the electrolytic tank." Proc. IEE., part IV, oct. 1951. Spencely. Smithsonian elliptic function tables. Washington, 1947.

SUBMITTED:

June 27, 1959.

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81379

S/108/60/015/05/07/008 B007/B014

9.3230

AUTHOR:

Ufel'man, A. F.

TITLE:

Synthesis of Electric Filters According to the Operating Parameters and With the Aid of Zolotarev's Fraction

PERIODICAL: Radiotekhnika, 1960, Vol. 15, No. 5, pp. 64-72

TEXT: The method of calculating filters according to the operating parameters and with the aid of Ye. I. Zolotarëv's isoextreme functions was developed by S. Darlington (Ref. 1) in 1939. Because of its complexity this method has not been applied. A. Grossman (Ref. 2) used the series of the A-functions to eliminate the elliptical functions from Darlington's formulas. However, also these formulas proved to be very extensive. The author of the present paper suggests simpler formulas for the calculation of filters. The special functions were eliminated by using E. Glowatzki's tables (Ref. 3). Thus, work could be largely reduced as compared to A. Grossman's formulas. Formula (1) is written down for the attenuation of some reactance four-terminal network consisting of linear lumped elements (Refs. 1, 4, and 5):

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81379

Synthesis of Electric Filters According to S/108/60/015/05/07/008 the Operating Parameters and With the Aid B007/B014 of Zolotarev's Fraction

 $e^{2A} = 1 + |\varphi|^2$ , A =  $\ln |S|$  - attenuation,  $S = \frac{g(\lambda)}{f(\lambda)}$  - transmission coefficient,  $\varphi = \frac{h(\lambda)}{f(\lambda)}$  - filtration function, f, g, and h - real polynomials

of the complex frequency  $\lambda = \sigma + i\omega$ . If f, g, and h are known, it is possible to find all parameters of the reactance four-terminal network and to determine its circuit. The electric filter is set up according to the attenuation in the following way: A filter circuit with the least number of elements is to be found, and the elements are used to prevent the attenuation from exceeding the rated value of  $A_{\max}$  within the range of transmission and from falling below the rated value of  $A_{\min}$  within the attenuation band. The three parts of the problem are enumerated: 1) determination of the filtration function  $g = \frac{h}{f}$ , 2) determination of the roots of the characteristic polynomial  $g(\lambda)$ ; 3) determination of the filter circuit from the resulting polynomials Card 2/3

Synthesis of Electric Filters According to the Operating Parameters and With the Aid of Zolotarev's Fraction

81379 S/108/60/015/05/07/008 B007/B014

f, g, and h. Next, the author describes the calculation of a standard low-frequency filter from which filters of the upper frequencies and band filters are obtained by means of frequency transformation. This calculation is illustrated by an example. It requires about as many operations as the calculation according to the characteristic parameters, but the quality of the filters is considerably improved. Mention is made of the Zobel filters and the general methods by P. L. Chebyshev. There are 2 figures and 13 references: 7 Soviet, 4 English, and 2 German.

SUBMITTED:

May 4, 1959 (initially) and May 21, 1959 (after revision)

Card 3/3

### "APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001857820007-3

CUFEL MAN, A.F.

Scientifically based study programs for training specialists in the field of radio engineering. Izv. vys. ucheb. zav.; radiotekh. 3 no.4: 520-521 Jl-Ag '60. (MIRA 13:10:

1. Kafedra elektrosvyszi Ural'skogo elektromekhanicheskogo instituta inzhenerov zhelezno-dorozhnogo transporta.

(Radio--Study and teaching)

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001857820007-3"

KAPELINSKIY, Yu.N.; POLYANIN, D.V.; MENZHINSKIY, Ye.A.; IVANOV, I.D.;

SERCHYEV, Yu.A.; KOSTYUKHIN, D.I.; DUDUKIN, A.N.; IVANOV, A.S.;

FINOGENOV, V.P.; ZAKHMATOV, M.I.; SOLODKIN. R.G.; DUSHEN'KIN, V.H.;

BOGDANOV, O.S.; SEROVA, L.V.; GONCHAROV, A.N.; KARKHIN, G.I.;

LYUBSKIY, M.S.; PUCHIK, Ye.P.; SEROVA, L.V.; KAMENSKIY, N.N.;

SABEL'NIKOV, L.V.; FEDOROV, B.A.; GERCHIKOVA, I.N.; KARAVAYEV, A.P.;

KARPOV, L.N.; SHIPOV, Yu.P.; VLADIMIRSKIY, L.A.; KUTSENKOV, A.A.;

RYABININA, E.D.; ANAN'YEV, P.G.; ROGOV, V.V.; BELOSHAPKIN, D.K.;

SEYFUL'MULYUKOV, A.M.; PAHFENOV, A.Ya.; SMIRNOV, V.P.; ALEKSEYEV,

A.F.; SHIL'UKRUT, V.A.; CHURAKOV, V.P.; BORISENKO, A.P.; ISUPOV, V.T.;

OHLOVA, N.V., red.; GORYUNOVA, V.P., red.; BELOSHAPKIN, D.K., red.;

GEORGIYEV, Ye.S., red.; KOSAREV, Ye.A., red.; KOSTYUKHIN, D.I., red.;

MAYOROV, B.V., red.; PANKIN, N.S., red.; PICHUGIN, B.M., red.;

POLYANIN, D.V., red.; SOLODKIN, R.G., red.; UFIMOV, I.S., red.;

EKHIN, P., red.; SMIRNOV, G., tekhn.red.

[Economy of capitalist countries in 1957] Ekonomika kapitalistichaskikh strah v 1957 godu. Pod red. N.V.Orlova, IU.N.Kapelinskogo
i V.P.Goriunova. Moskva, Izd-vo sotsial no-ekon.lit-ry, 1958.

(MIRA 12:2)

1. Moscow. Nauchno-issledovatel'skiy kon"yunkturnyy institut.
(Economic conditions)

POTEKHIN, I.I., glav. red.; BARANOV, A.N., red.; BELYAYEV, Ye.A., red.; GELLER, S.Yu., red.; GRAVE, L.I., st. nauchnyy red.; GRIGOR'YEV, A.A., red.; GUEER, A.A., red.; KULAGIN, G.D., red.; MALIK, YA.A., red.; MANCHKHA, P.I., red.; MILOVANOV, I.V., red.; NERSESOV, G.A., red.; OL'DEROGGE, D.A., red.; ORLOVA, A.S., red.; POPOV, K.M., red. ROZIN, M.S., kand. ekon. nauk, red.; SMIRNOV, S.R., red.; UFIMOV, I.S., red.; SHVEDOV, A.A., red.; YASTREBOVA, I.P., red.; PAVLOVA, T.I., tekhn. red.

[Africa; encyclopedia] Afrika; entsiklopedicheskii spravochnik. Glav. red. I.I.Potekhin. Chleny red. kollegii: A.N.Baranov i dr. Moskva, Vol.1. A - L. 1963. 474 p. (MIRA 16:4)

1. Sovetskaya entsiklopediya, Gosudarstvennoye nauchnoye izdatel'stvo, Moscow.

(Africa--Dictionaries and encyclopedias)

UFIMISEV, A.M., inzh.

Testing of water-wheel generators. Elek.sta. 29 no.5:49-51 My '58.

(MIRA 12:3)

(Electric generators--Testing)

UFINITERY, A.M., inch.

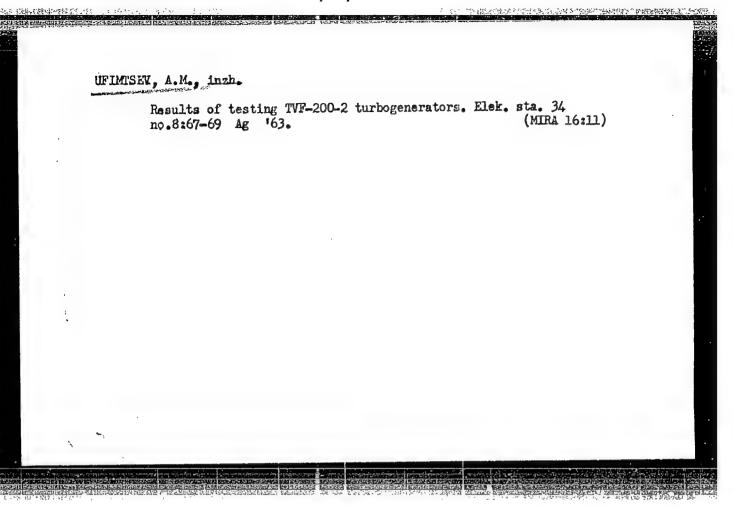
Increase of hydrogen pressure in TV2.100-2 and TV-50-2 turbogenerators. Energetik 10 no.1:19-22 Ja '62.

(MIRA 14:12)

(Turbogenerators)

UFINTSEV, A.M., inzh.; LEBEDEV, A.T., inzh.

Testing of turbogenerators in asynchronous operation. Elek. sta. 33 no.8:28-32 Ag '62, (MIRA 15:8) (Turbogenerators—Testing)



S/139/60/000/03/042/045

Vorob'yev, A.A., Savintsev, P.A. and Ufimtsev, B.F. AUTHORS:

TITLE:

The Ionisation Potentials of Atoms and the Mutual

Solubility of Metals

PERIODICAL:

Izvestiya vysshikh uchebnykh zvedeniy, Fizika,

1960, No 3, pp 233 - 234 (USSR)

ABSTRACT:

Depending on the type of interaction between the components, fused metals can form various types of alloys, e.g. eutectic mixtures, solid solutions or chemical compounds. It is well known that there is a definite periodicity in the ionisation potentials of elements, depending on their position in the periodic It is argued that intermetallic compounds! are formed when the ionisation potentials of the two metals are considerably different. Conversely, in the case of eutectic alloys, the ionisation potentials of the components are roughly the same. Solid solutions are formed when the difference between the ionisation potentials of the components approach a certain average value. These ideas are illustrated in Table 1, in which eutectic alloys are shown on the left and solid solutions

Card1/2

The Ionisation Potentials of Atoms and the Mutual Solubility of

on the right.  $\phi_1$ and  $\phi_2$  are the ionisation potentials and  $\Phi \phi$  is the difference between them. There are I table and 2 Soviet references.

ASSOCIATION: Tomskiy politekhnicheskiy institut imeni S.M. Kirova (Tomsk Polytechnical Institute imeni S.M. Kirov)

SUBMITTED: October 26, 1959

Card 2/2

CIA-RDP86-00513R001857820007-3" APPROVED FOR RELEASE: 04/03/2001

SAVINTSEV, P.A.; UFIMTSEV, B.F.

Contact melting of multicomponent organic systems. Izv. TPI 105:215-217 '60. (MIRA 16:8)

1. Predstavleno nauchnym seminarom radiotekhnicheskogo fakuliteta Tomskogo ordena Trudovogo Krasnogo Znameni politekhnicheskogo instituta imeni Kirova. (Melting)

### UFINTSEV, F.

Great changes. Mast.ugl. 5 no.4:10-12 Ap '56. (MLRA 9:7)

l.Nachal'nik Bachatskogo razreza kombinata Kuzbassugol'. (Kuznetsk Basin--Ship mining)

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001857820007-3"

UFIMTSEV, G. N.

Proyektirovaniye promyshlennykh predpriyatiy (Designing industrial enterprises)
Moskva, Gos. Izd-vo Literatury po Stroitel'stvu i Arkhitekture, 1952.

198 p. illus., diagrs., tables.
At head of title: M. L. Zaslav, V. N. Zlatolinskiy, A. E. Levinson, T. G. Petrova,
G. N. Ufimtsev, P. M. Frenkel.

N/5 748.11 .F8

也是是有关键的。

UFIMITSEV, G.N.

POLYAKOV. D.L., inzhener, redaktor; BATURIN, V.V., kandidat tekhnicheskikh nauk, redaktor; BORISOV, V.P., inzhener, redaktor; GOVOROV, V.P., inzhener, redaktor; MATS, Ya.M., inshener, redaktor; RYVKIN, Kh.I., kandidat tekhnicheskikh nauk, redaktor; TURKUS, V.A., dotsent, redaktor; KORSA-KOV. S.S., retsensent; UFIMTSEV, G.N., retsensent. 

[Manual for planning heating and ventilation systems of industrial enterprises, Spravochnik po proektirovaniju otoplenija i ventiliatsij promyshlennykh predpriiatii. [Radkollegiia D.L. Poliakov i dr. Redaktor Y.A. Turkus] Moskva, Gos. izd-vo lit-ry po stroitel'stvu i arkhitekture,

1. Leningrad Proyektnyy institut ministerstva stroitel stva. (Heating-Handbooks, manuals, etc.) (Ventilation-Handbooks, manuals,

KISSIN, Mikhail Isakovich, dotsent, kandid

KISSIN, Mikhail Isakovich, dotsent, kandidat tekhnicheskikh nauk, [deceased];
MAZO, A.V., inzhener, retsenzent; UL'YANINSKIY, S.V., professor, doktor
tekhnicheskikh nauk, retsenzent; UFINTSKY, G.N., inzhener, retsenzent,
redaktor; GOLUBENKOVA, L.A., redaktor; HEDVEDEV, L.Ya., tekhnicheskiy
redaktor

[Heating and ventilating] Otoplenie i ventiliatsiia. Izā.2-ce, perer. Moskva, Gos.izd-vo lit-ry po stroitel\*stvu i arkhitekture. Pr.1. [Heating] Otoplenie. 1955. 390 p. (MLRA 9:3) (Heat engineering)

KYUBLER, O.A., inzh., red.; UFINTSEV, G.N., inzh., red.; GRIGOR'YEV, P.G., red.; TOL', A.O., red.; MUNITS; A.P., red.izd-va; BOROVNEV, N.K., tekhn.red.; SOLNTSEVA, L.M., tekhn.red.

[Unified standards for planning and survey work paid by a piece-rate] Edinye normy vyrabotki na proektnye i izyskatel'skie raboty, oplachivaemye sdel'no. Moskva, Gos.izd-vo lit-ry po stroit., arkhit. stroit.materialam. Pt.2. [Industrial buildings and structures] Pro-tary-engineering installations for buildings and structures] Vnut-rennic sanitarno-tekhnicheskie ustroistva zdenii i sooruzhenii. 1958. Kopiroval'nye raboty. 1958. lut p. (MIRA 12:12)

1. Russia (1923- U.S.S.R.) Gosudarstvennyy komitet po delam stroitel'stva. (Building--Production standards)

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001857820007-3"

BELOUSOV, Vladimir Vladimirovich, inzh.; MIKHAYLOV, Fedor Semenovich, inzh.; SMIRNOV, L.I., inzh., nauchnyy red.; UFIMTSEV, G.N., inzh., red.; SAFONOV, P.V., red. izd-va; RODIONOVA, V.M., tekhm. red.

[Principles of the design of central heating systems]Osnovy proektirovaniia sistem tsentral'nogo otopleniia. Moskva, Gosstroiizdat, 1962. 401 p. (MIRA 15:12)

KISELEV, G., mayor; TOPIL'SKIY, V., mayor; GLUSHKIN, I., starshina; UFIMTSEV, I., kapitan; PROKOP'YEV, G., starshiy leytenant; DEREVYANKO, N., leytenant

How do you train radiotelegraph operators?; discussion of the article published in No.1. Voen. vest. no.3: 101-103 Mr 64. (MIRA 17:5)

SUD-ZLOCHEVSKIY, A.I. [Sud-Zlochevs'kyi, A.I.] (Kiyer); UFIMTSEV, I.G. [Ufimtsev, I.H.) (Kiyev)

Method for optimizing a transient process in a servosystem with an escillatory drive of the third order. Avtomatyka 8 no.6:3-10 \*63. (MIRA 17:8)

POLESHCHUK, V. Ye., kand. istoricheskikh nauk, dotsent, mayor; KUSH-NEROV, P.I., podpolkovnik; YAKOVLEV, V.N., kapitan 2-go range; DMITRIYEV, V.A., kapitan 3-go range; UFIMTSEV, L. Ya., red.; MIRKISHIYEVA, S., tekhn. red.

[The fighting and revolutionary traditions of the sailors of the Red Banner Caspian Fleet] Boevye i revolutsionnye traditsii zhanskoe gos. izd-vo. 1960. 178 p. (MIRA 14:5)

UFIMTSEV, N.I.; TRENIKHIN, O.K.

At the electrified a.c. sections of the Krasnoyarsk railroad. Elek. i tepl. tiaga 5 no.3:28-29 Mr '61. (MIRA 14:6)

Nachal'nik distantsii kontaktnoy seti st. Bazaikha (for Ufimtsev).
 Nachal'nik Krasnoyarskogo uchastka energosnabzheniya (for Trenikhin).
 (Electric railroads)

UFIMTSEV, N.I., inzh.

Some methods of work on the a.c. overhead contact system.
Elek.i tepl.tiaga 6 no.4:10-11 Ap :62. (MIRA 15:5)

(Electric railroads--Maintenance and repair)

Motortrucks at the 3rd International Fair in Danascus. Avt.transp.
35 nc.6:37 Je '57. (MIRA 10:7)

(Danascus--Faira--Motortrucks)

Ulimisev. R. YA.

AUTHOR: TITLE:

Ufimtsev, P. Ya.

An Approximative Calculation of Diffraction of Plane Electro-magnetic Waves on Some Metallic Bodies. I. Wedge and Band Diffraction (Ariblishenny) reschet diffraktsii ploskikh elektro-magnitnykh voln na nekotorykh

metallicheskikh telakh. I Diffraktsiya na kline i lente) PERIODICAL: Zhurnal Tokhn.Fiz. 1957, Vol 27, Nr 8, pp 1840-1849(USSR)

ABSTRACT:

Approximate methods are of great importance as the exact solutions of the diffraction problems for complicated bodies meet with great mathematical difficulties. The author starts from the idea that a field diverged by the body can be taken as a sum of two current components flowing on the surface. The one component is the uniform one which obeys to the laws of geometrical optics, the field of which can be found by means of quadratures, and which represents the so-called Kirchhoff approach. The nonuniform component is that current which is added to the uniform one in connection with the surface curvature. In the case of convex bodies the nonuniform component can be assumed on a sufficiently small element of the convex surface in the neighborhood of the break and approximately equal to that of the corresponding dihedral angle (wedge). The diffraction is investigated with a wedge and a band, either of them perfectly conductive, and an approximate calculation of them is carried out. The method given here can also be

Card 1/2

An Approximative Calculation of Diffraction of Plane Electromagnetic Waves on Some Metallic Bodies. I. Wedge and Band

used for wave lengths which are by far smaller than the measurements of linear bodies, and this also in the case of a sufficiently great distance from the bodies. There are 9 figures

SUBMITTED: AVAILABLE:

July 30, 1956 Library of Congress

Card 2/2

AUTHOR:

Ufimtsev, P. Ya.

57-28-3-21/35

TITLE:

Secondary Diffraction of Electromagnetic Waves on a Band (Vtorichnaya diffraktsiya elektromagnitnykh voln na lente)

PERIODICAL:

Zhurnal Tekhnicheskoy Fiziki, 1958, Vol. 28, Nr 3,

pp. 569-582 (USSR)

Same of a

ABSTRACT:

The approximation method for solving the diffraction problems earlier developed in references 1 and 2 is precisely defined here. The so-called effect of the secondary diffraction, i. e. the interaction of currents flowing in the different elements of the body surface is taken into account here. The dispersing object can be approximated by a number of sources - luminous lines and points. The problem posed here consists in the fine ding of those functions which determine the continuous modifi= cations of the field of each of those sources on transition through the corresponding light-shadow-boundary. This problem is here investigated in application to the simplest body- a band - and more accurate formulae for the dispersing field are

Card 1/2

obtained. In the case of the diffraction on a band the part

Secondary Diffraction of Electromagnetic Waves on a Band

57-28-3-21/33

played by the above-mentioned interaction is most essential in the direction of observation near the band-plane as well as in the case of grating incidence of the irradiating wave. Approximation formulae for the field dispersed by the band are derived which are useful for any directions of radiation and observation. Computations of the disperion characteristics according to the exact and the approximation theory are performed and then a comparison of the two is given. The results show a satisfactory agreement between the approximation method and the exact theory already at  $kz = \sqrt{28}$ , although in this case only about two and a half wave lengths come to lie on the width of band. The work was guided by L. A. Vaynshteyn.

There are 13 figures, and 4 references, 3 of which are Soviet.

SUBMITTED:

March 25, 1957.

1. Electromagnetic waves—Diffraction 2. Electromagnetic waves—Electrical factors 3. Mathematics

Card 2/2

UFIMTSEY, P.Ya.

45.44

Approximate calculation of the diffraction of plane electromagnetic waves on some metallic surfaces. Part 2: Diffraction en a disk and a finite cylinder. Zhur. tekh. fiz. 28 no.11:2604-2616 N '58.

(MIRA 12:1)

(Electric waves-Diffraction)

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001857820007-3"

生物学的 新军工

AUTHOR:

Ufimtsev, P. Ya.

57-28-3-22/33

TITLE:

Secondary Diffraction of Electromagnetic Waves on a Disk (Vtorichnaya diffraktsiya elektromagnitnykh voln na diske)

PERIODICAL:

Zhurnal Tekhnicheskoy Fiziki, 1958, Vol. 28, Nr 3,

pp. 583-591 (USSR)

ABSTRACT:

The approximate solution of the diffraction problem for a disk found earlier (reference 1) is precisely defined here. The interaction of the boundary currents is approximately taken into account here. Equations for the field dispersed by the disk are derived. The dispersion characteristics are computed and compared with the results of the exact theory and those of the experiment. A satisfactory agreement with the experiment is determined. The taking into account of the interac= tion of the boundary currents precisely defines the approxima= tion given earlier and is in better agreement with the exact

theory.

The work was guided by L. A. Vaynshteyn.

Card 1/2

There are 6 figures, and 3 Soviet references.

Secondary Diffraction of Electromagnetic Waves on a Disk 57-23-3-22/33 SUBMITTED: March 25, 1957.

1. Electromagnetic waves--Diffraction 2. Mathematics

Card 2/2

9,9300

\$/109/60/005/012/008/035 E032/E514

AUTHORS:

Mayzel's, Ye. N. and Ufimtsev, P. Ya.

TITLE &

Reflection of Circularly Polarized Electromagnetic Waves

from Metal Bodies

PERIODICAL: Radiotekhnika i elektronika, 1960, Vol.5, No.12,

pp,1925-1928

TEXT: The Kirchhoff method is frequently used to treat the reflection of electromagnetic waves by metal bodies. According to this method the scattered field is produced by a surface current given by

 $\vec{j} = \frac{c}{2\pi} \left[ \vec{nH} \right],$ (1)

is the velocity of light in vacuo, n is the outward normal to the surface of the body and H is the magnetic field of the incident wave. Physically Eq.(1) means that at each element of area on the "illuminated" surface the current is considered to be the same as/an infinite, perfectly conducting plane tangent to the given However, this formula does not take into account additional currents due to the curvature of the surface. surface current must be looked upon as a sum of the "uniform" Card 1/3

20410 s/109/60/005/012/008/035

Reflection of Circularly Polarized Electromagnetic Waves from Metal Bodies

current component given by Eq.(1) and a "nonuniform" component due The Kirchhoff approximation must, therefore be abandoned whenever the nonuniform component is of interest. second of the present authors has developed methods which could be used in this connection. In many cases, however, a direct calculation is difficult and it is, therefore, desirable to develop a method which could be used to measure the nonuniform component of such measurements can be carried out for rigid bodies of revolution It is shown in the present paper that with the aid of circularly polarized electromagnetic waves. It is shown that when such bodies are irradiated with circularly polarized electromagnetic waves, the nonuniform components in the scattered field can be separated out with the aid of a polarizer. calculations have been carried out for a flat disc having a diameter of the order of the wavelength. (Fig. 3) were found to be in good agreement with experimental results, The numerical calculations The discrepancy between the two curves is partly due to the fact that

201.10

s/109/60/005/012/008/035 E032/E514

Reflection of Circularly Polarized Electromagnetic Waves from

in the experimental part a truncated conical specimen instead of a disc was employed. There are 3 figures and 3 Soviet references.

SUBMITTED: March 26, 1960

Card 3/3

9,3700 (1057,1163,1482 AUTHOR:

S/109/61/006/004/007/025 E032/E135

Ufimtsev, P.Ya.

TITLE:

Symmetrical Irradiation of finite bodies of revolution PERIODICAL: Radiotekhnika i elektronika, Vol.6, No.4, 1961,

TEXT: The diffraction of electromagnetic waves by perfectlyconducting finite bodies with surface discontinuitite is of considerable interest but, in view of its complexity, has not so far been fully investigated. In the case of radio waves whose wavelength is short in comparison with the linear dimensions of the diffracting object, it is usual to employ the Kirchhoff approximation. It is stated that this approximation frequently leads to incorrect results and should be improved. In the special case of convex solids of revolution irradiated along the axis of symmetry, the present author has found an improved approximation for the effective surface (Ref. 1: ZhTF, 1957, 27, 8, 1840, and Ref. 2: ZhTF, 1958, 28, 11. 2604). The method employed in the calculation has been described in the mentioned papers. scattered field is determined as a sum of "uniform" and

S/109/61/006/004/007/025 E032/E135

Symmetrical irradiation of finite bodies of revolution

"nonuniform" components. The uniform component represents the scattered field on the Kirchhoff approximation and is found to be integrating the surface current

$$\vec{j} = \frac{c}{2\pi} \left[ \vec{n} \vec{H} \right]$$

where; c is the velocity of light in vacuum; n is the output normal to the surface; and n is the magnetic field of the incident wave. The nonuniform component is an additional field due to the discontinuity and must be taken into account if one is to obtain correct results. The theory developed in Refs.1 and 2 is now extended to the case of a cone and a paraboloid of revolution (r<sup>2</sup> = 2pz). The author calculates the effective scattering surface of a finite cone and a paraboloid of revolution. The linear dimensions of the bodies are assumed large in comparison with the wavelength, with ideally conducting surfaces. The author finds that the shape of the body in the shadow region card 2/4

S/109/61/006/004/007/025 E032/E135

Symmetrical irradiation of finite bodies of revolution

wavelengths from the edge of the shadow. While the expressions found are in good agreement with experimental results, even for large dimensions, they do not pass into the formulae of physical optics. At the same time they differ from the results of the Kirchhoff approximation, which does not agree too closely with Thus, for example, Fig. 4 shows a plot of  $\log \sigma$ (o is the effective scattering area) as a function of the length of the cone. The points are experimental and the dashed curve represents the Kirchhoff approximation and the full curve the present results. Acknowledgements are expressed to Ye.N. Mayzel's and L.S. Chugunova for their assistance. There are 10 figures and 5 references: 2 Soviet and 3 non-Soviet.

SUBMITTED: April 28, 1960

Card 3/4

CIA-RDP86-00513R001857820007-3" APPROVED FOR RELEASE: 04/03/2001

30443 \$/109/61/006/012/018/020 D201/D305

9,1912

AUTHOR: Ufimtsev, P.Ya.

TITLE: Reflection of circularly polarized radiowaves from

metal bodies

MERIODICAL: Radiotekhnika i elktronika, v. 6, no. 12, 1961,

2094 - 2095

TEXT: E.N. Mayzel's and P.Ya. Ufimtsev, suggested (Mef. 1: Radiotekhnika i elektronika, 1960, 5, 12, 1925) a method for measuring the 'irregular' component of the field dispersed by metal bodies of revolution. In the present short communication it is shown that this method may be applied for measuring the irregular field component of the field, dispersed by metal objects of finite dimensions of any shape. The system of coordinates is chosen so that the normal N to the incident wave front, drawn through the origin be in plane yoz as shown in Fig. 1. It is easy to show that with E-polarization (E yoz) the current density induced at the body surface by the incident wave is given in the Kirchhoff approximation Card 1/4%

30h43 S/109/61/006/012/018/020 D201/D305

Reflection of circularly polarized ...

by

$$i_x = -\frac{c}{2\pi} E_{0x} (n_y \sin \gamma + n_z \cos \gamma) e^{i\Psi},$$

$$i_y = \frac{c}{2\pi} E_{0x} n_x \sin \gamma e^{i\Psi},$$
(1)

$$i_{x} = 0,$$

$$i_{y} = \frac{\sigma}{2\pi} H_{0x} n_{z} e^{i\Psi},$$

$$i_{z} = -\frac{c}{2\pi} H_{0x} n_{y} e^{i\Psi},$$
(2)

for an H-polarized wave  $(\overrightarrow{H}_0 \perp yoz)$  where C - velocity of light in vacuum;  $\overrightarrow{E}_{ox}$  and  $\overrightarrow{H}_{ox}$  - amplitudes of the el. and magn. components of the incident wave for E and H polarization respectively;  $\psi = K(y')$  sin  $\gamma + z'$  cos  $\gamma$ ) - the phase of the incident wave at point (x', y') at body surface;  $\overrightarrow{n}_x$ ,  $\overrightarrow{n}_y$ ,  $\overrightarrow{n}_z$  - components of the normal to the surface at the same point. The time dependence is assumed to be  $e^{-i\omega t}$ . In radio telemetry, when the direction of observation and Card  $2/\sqrt{3}$ 

5/109/61/006/012/018/020 D201/D305

Reflection of circularly polarized ...

transmission usually coincide, (the spherical coordinates of the point of observation being R,  $\theta$ ,  $\varphi$ ) so that  $\hat{\theta} = \Re - \gamma$ ,  $\varphi = - \Re/2$ , expressions

 $E_x = -H_0 = \frac{iaB_{0x}}{2} \, \overline{\Sigma_k} \, \frac{e^{ikR}}{R} \, , \ E_0 = H_x = 0$ (3a)

$$H_x = E_{\theta} = \frac{ia H_{0x}}{2} \sum_k \frac{e^{ikR}}{R}, \quad E_x = H_{\theta} = 0.$$
 (4a)

hold. The factor a in these expressions represents an arbitrary linear dimension of the body, and functions  $\Sigma_k$  and  $\overline{\Sigma}_k$  are determined ned by

 $\Sigma_{k} = -\overline{\Sigma}_{k} = \frac{k}{\pi a} \int (n_{y} \sin \gamma + n_{z} \cos \gamma) e^{i\Phi} dS.$ (5)

Thus the equality  $\Sigma_k = -\overline{\Sigma}_k$  is satisfied for any body shape and the method described in (Ref. 1: Op.cit.) has a general meaning and permits isolation from the field, dispersed by a metal body. There are 1 figure and 1 Soviet-bloc reference. June 10, 1961 SUBMITTED: Card 3/4/3

UFIMTSEV, Petr Yakovlevich: IVANUSHKO, N.D., red.; SVESHNIKOV, A.A., tekhn. red.

[Edge wave method in physical diffraction theory] Metod kraevykh voln v fizicheskoi teorii difraktsii. S predisl. L.A. Vainshteina. Moskva, Sovetskoe radio, 1962. 242 p.

(MIRA 16:4)

APPROVED FOR RELEASE: 04/03/2001

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34491 s/109/62/007/002/010/024 D266/D303

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Ufimtsev. P.Ya.

TITLE:

AUTHOR:

Scattering of a plane electromagnetic wave by a thin

cylindrical conductor

PERIODICAL:

Radiotekhnika i elektronika, v. 7, no. 2, 1962, 260 - 269

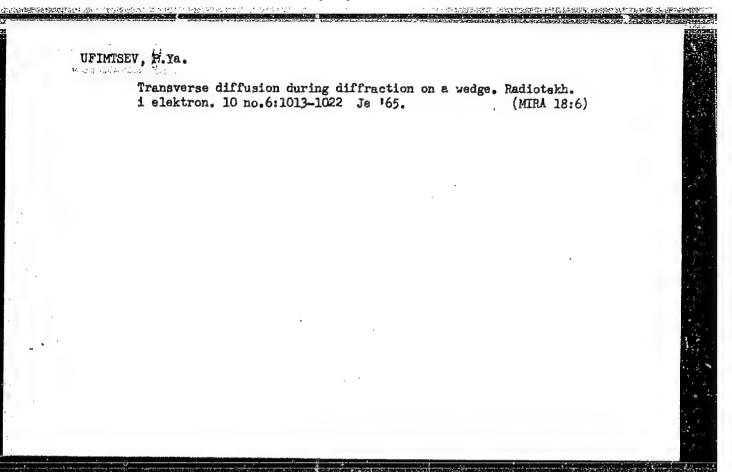
TEXT: The purpose of the paper is to study the scattering effect of a cylindrical conductor of radius  $\alpha$  and length L. The direction of the incident plane electromagnetic wave is given by the angle  $\hat{V}_0$  of the polarization of the wave by  $\alpha$ , ( $\alpha$  = 0 if the electric vector the polarization of the wave by  $\alpha$ , the direction of observation by  $\hat{V}_0$ . The author's calculations are based on the following physical picture: The incident plane wave excites certain waves (called "edge" waves) which are scattered on the opposite end of the conductor waves, which are scattered on the opposite end of the condition and cause the excitation of secondary "edge" waves. These secondary waves excite ternary waves, etc. The first order term is given by the expression

Card 1/2

S/109/62/007/002/010/024 Scattering of a plane electromagnetic.. D266/D303

$$E_{\theta}^{(1)} = H_{\varphi}^{(1)} = - E_{\theta}^{ikR} F^{(1)}(\theta_0, \theta), \qquad (3)$$

where R - distance of the point of observation,  $k=2\pi/\lambda$ ,  $\lambda$  - wavelength and  $F(1)(\vartheta_0,\vartheta)$  can be determined by employing L.A. Vaynshteyn's variational principle (Ref. 4: ZhTF, 1961, 31, 1, 29). Summing all the contributions up to infinity the resultant field strength in the far field is obtained. The resulting formula is lengthy and complicated, but two important conclusions can be immediately drawn: 1) If  $L = n(\lambda/2)$  resonance occurs; 2) The formula is invariant in respect of a change of  $\vartheta$  and  $\vartheta_0$ . This last property follows from the reciprocity theorem. The author claims that in previous treatments - due to different approximations - reciprocity was not satisfied and his is the first solution which comes to the correct result. There are 4 figures and 7 references: 5 Soviet-bloc and 2 non-Soviet-bloc. The references to the English-language publications read as follows: K. Lindroth, Trans. Roy. Inst. of Technol., Stockholm, 1955, no. 91; J.H. Van Vleck, F. Bloch, M. Hamermesh, J. Appl. Phys., 1947, 18, 3, 274. SUBMITTED: June 10, 1961 Card 2/2



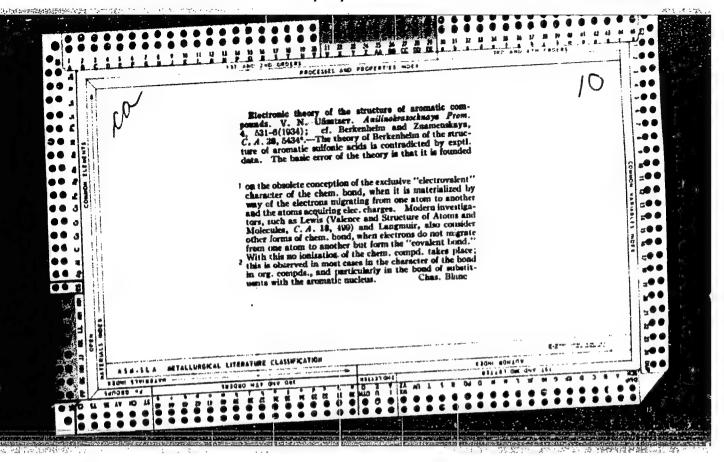
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AUTHOR: Fistul', V. I.; Omel'yanovskiy, E. M.; Pelevin, O. V.; Ufimtsev, V. B.	
ORG: Giredmet	
TITLE: The effect of the nature of dopant on electron scattering and polytropy of	
SOURCE: AN SSSR. Izvestiya. Neorganicheskiye materialy, v. 2, no. 4, 1966, 657-658	
TOPIC TAGS: gallium arsenide, single crystal, semiconductor single crystal, activated crystal, donor impurity, electron mobility, carrier scattering, Hall mobility, impurity polytropy	
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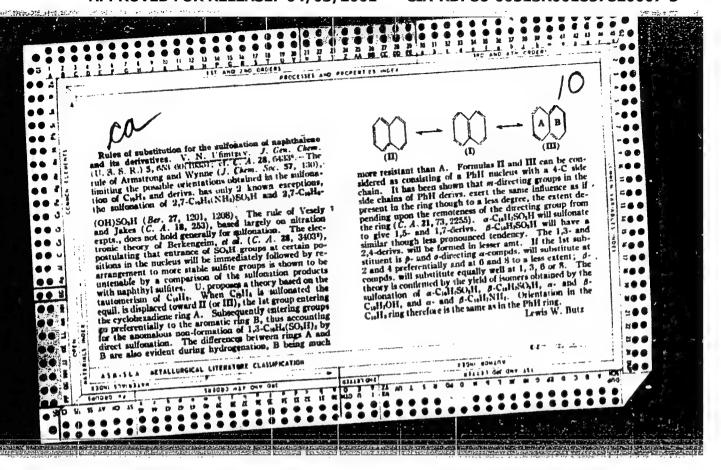
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UFIMTSEV, V. D., and KOZLOV, I. Ya.

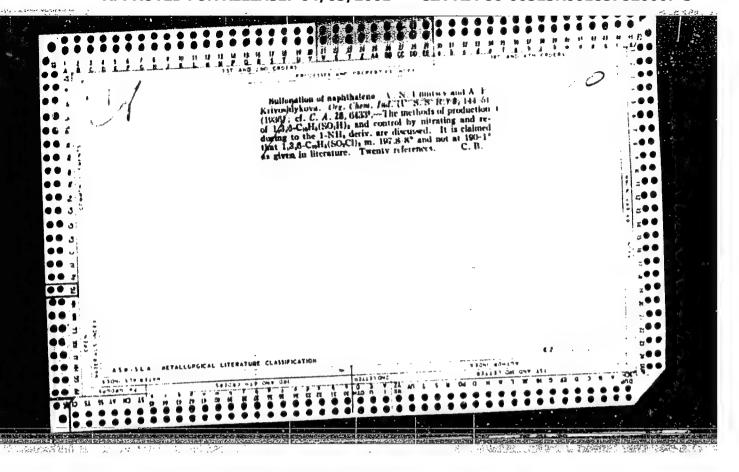
"Characteriestics of the Heat Treatment of Cast Alloys to Be Used for Permanent Magnets." From the book, "Heat Treatment and Properties of Cast Steel." edited by N. S. Kreshchanovskiy, Mashgiz, Moscow 1955.

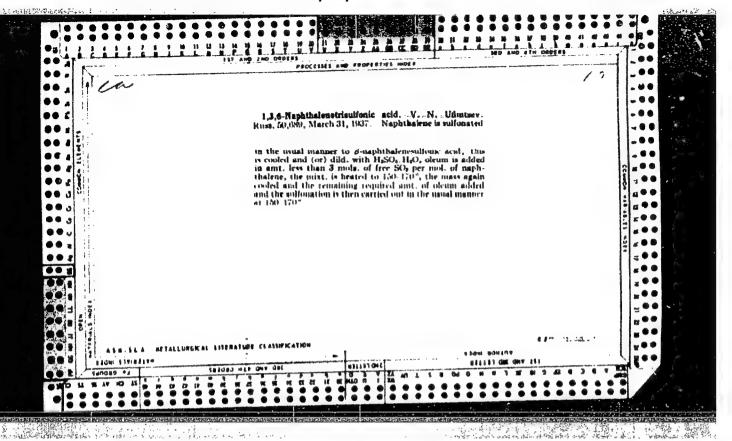


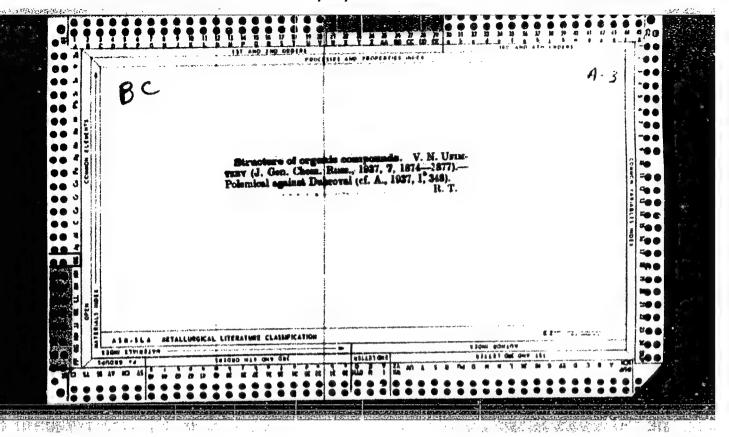


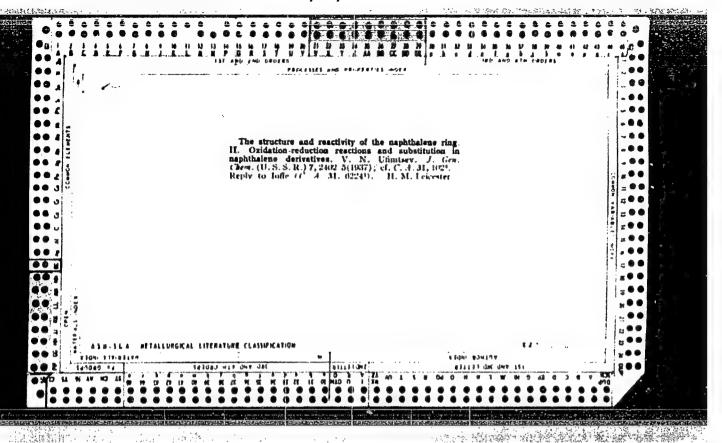
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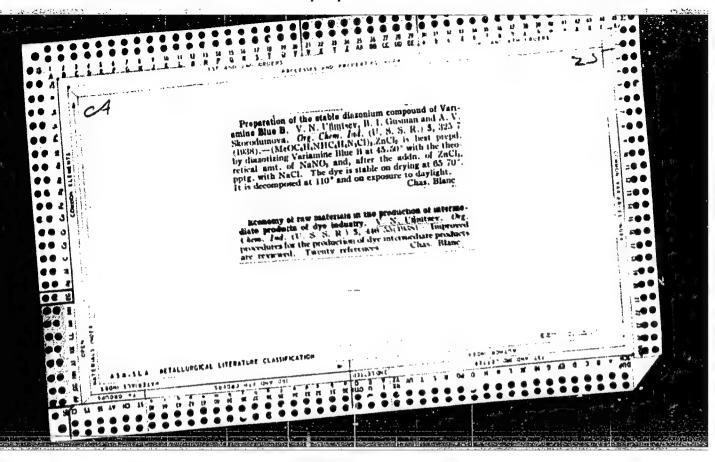
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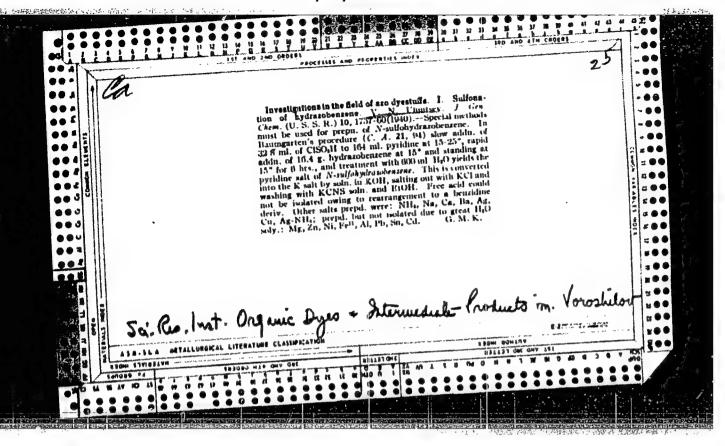


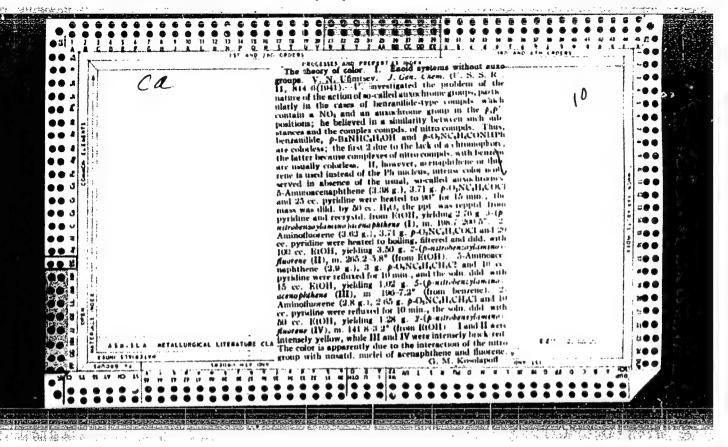




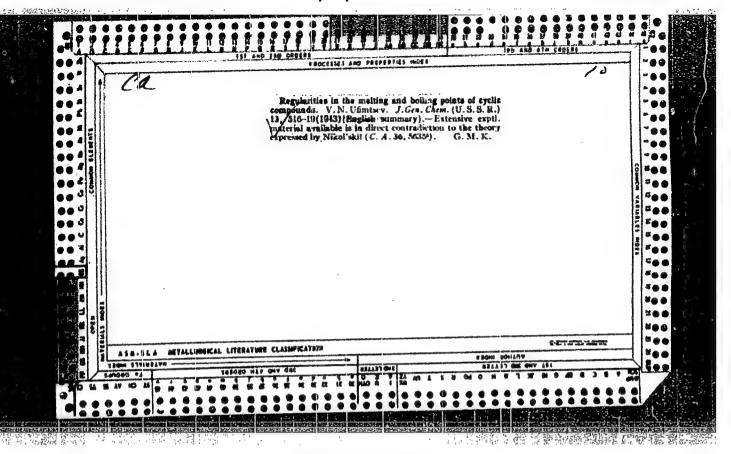


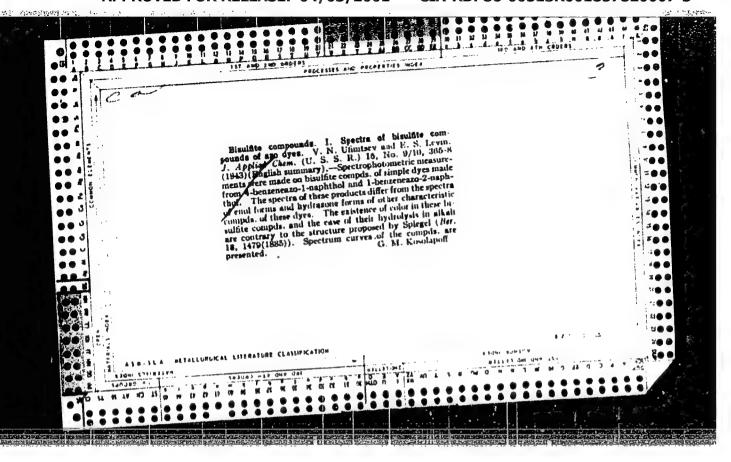


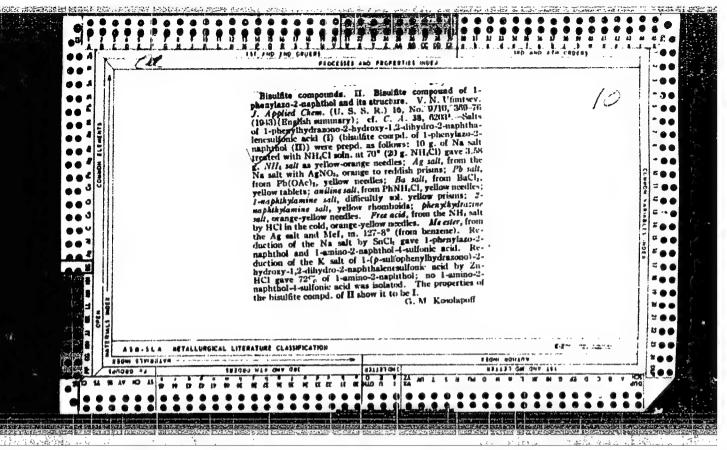






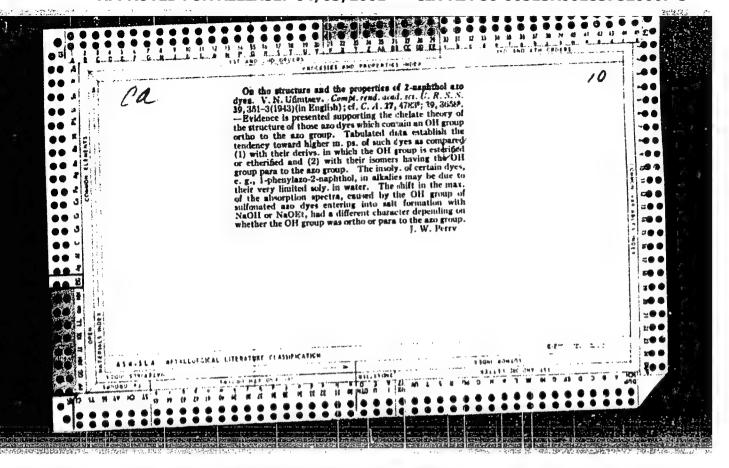


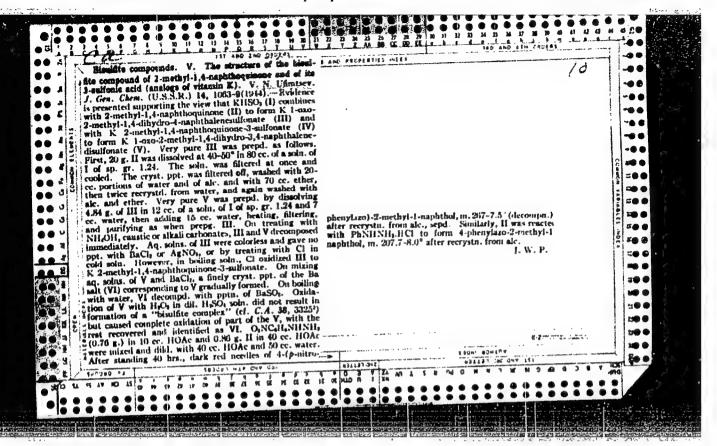


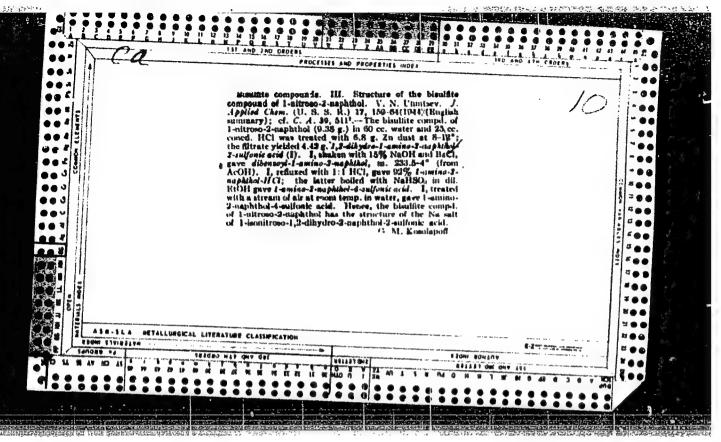


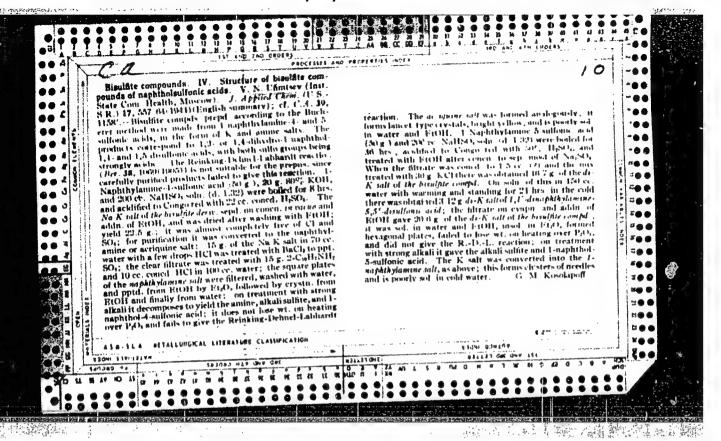
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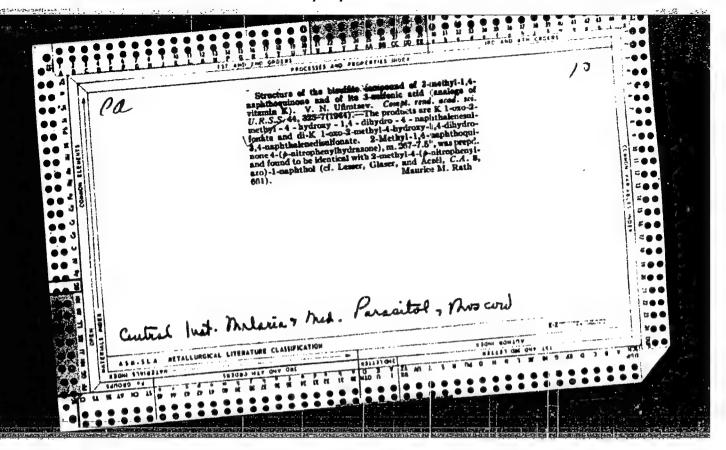


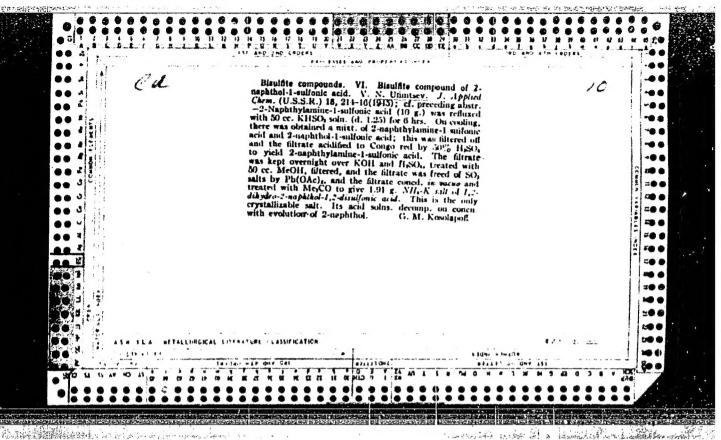


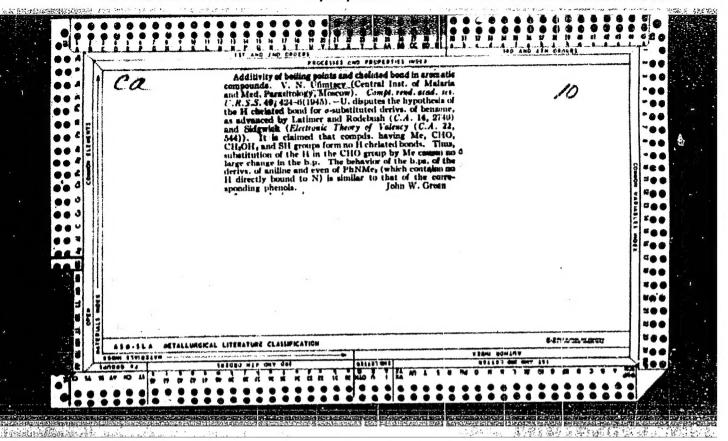


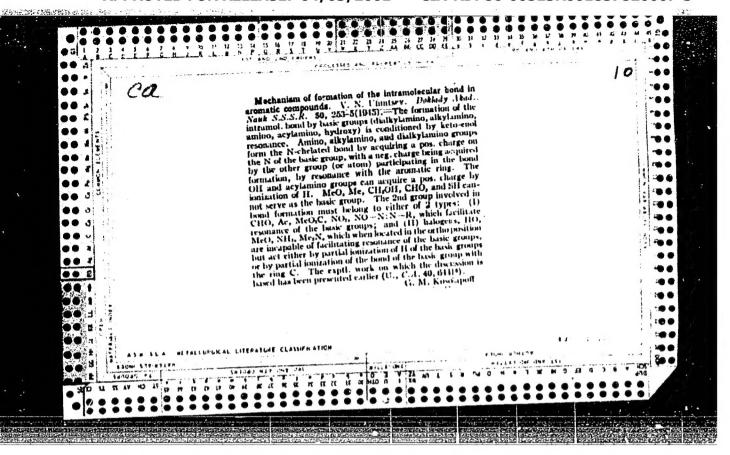
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"The reaction capacity of the narhthalene nucleus in the light of resenance conceptions" by V. N. Ufintzev (p. 750)

SO: Journal of General Chemistry (Zhurnal Obshchei Khimii) 1946, Volume 16, No. 4-5

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